

# The higher-order gradient model for large-eddy simulation of turbulent flows

Maurits H. Silvis

*Supervisors*

Roel W.C.P. Verstappen

Arthur E.P. Veldman

July 22, 2014



university of  
groningen

faculty of mathematics  
and natural sciences

johann bernoulli institute for  
mathematics and computer science

## Overview

- Research aim
- Large-eddy simulation
- The gradient model
- The higher-order gradient model
- Numerical results
- Conclusions and future work

## Description of incompressible flows

- Navier-Stokes equations

$$\frac{\partial u_i}{\partial x_i} = 0$$

$$\frac{\partial u_i}{\partial t} + \frac{\partial}{\partial x_j} (u_i u_j) = -\frac{\partial p}{\partial x_i} + \frac{1}{Re} \frac{\partial^2 u_i}{\partial x_j \partial x_j}$$

- Filtered Navier-Stokes equations

$$\frac{\partial \bar{u}_i}{\partial x_i} = 0$$

$$\frac{\partial \bar{u}_i}{\partial t} + \frac{\partial}{\partial x_j} (\bar{u}_i \bar{u}_j) = -\frac{\partial \bar{p}}{\partial x_i} + \frac{1}{Re} \frac{\partial^2 \bar{u}_i}{\partial x_j \partial x_j} - \frac{\partial}{\partial x_j} \underbrace{(\overline{u_i u_j} - \bar{u}_i \bar{u}_j)}_{\tau_{ij}}$$

## Description of incompressible flows

- Filtering

- Convolution product:

$$\bar{u}_i(\vec{x}, t) = \int u_i(\vec{x}', t) G(\vec{x} - \vec{x}') d\vec{x}'$$

- Box filter

$$G(\vec{x} - \vec{x}') = \frac{1}{\delta^3} \begin{cases} 1 & \text{if } |\vec{x} - \vec{x}'| \leq \frac{\delta}{2} \\ 0 & \text{otherwise} \end{cases}$$

- Filter length:  $\delta$

## The gradient model

- “Approximate deconvolution method based on wavenumber asymptotics”
- Derivation

$$\tau_{ij} = \underbrace{\overline{u_i u_j} - \bar{u}_i \bar{u}_j}_{\#1}$$

$$\tau_{ij} = \underbrace{\overline{\bar{u}_i \bar{u}_j} + \overline{\bar{u}_i u'_j} + \overline{u'_i \bar{u}_j} + \overline{u'_i u'_j}}_{\#2} - \bar{u}_i \bar{u}_j$$



$$\mathcal{F}$$

$$\sum_{m=0}^n \dots \delta^n$$

$$\mathcal{F}^{-1}$$

Fourier transform

Taylor expansion in the filter length

Inverse Fourier transform



$$\underbrace{\tau_{ij} = f(\mathbf{u}_k)}_{\#1} + \mathcal{O}(\delta^{n+2})$$

$$\underbrace{\tau_{ij} = g(\bar{\mathbf{u}}_k)}_{\#2} + \mathcal{O}(\delta^{n+2})$$

## The gradient model

$$\underbrace{\tau_{ij} = \frac{1}{12} \delta^2 \frac{\partial u_i}{\partial x_k} \frac{\partial u_j}{\partial x_k} + \mathcal{O}(\delta^4)}_{\#1}$$

$$\underbrace{\tau_{ij} = \frac{1}{12} \delta^2 \frac{\partial \bar{u}_i}{\partial x_k} \frac{\partial \bar{u}_j}{\partial x_k} + \mathcal{O}(\delta^4)}_{\#2}$$

- Problems
  - Numerically unstable
  - Turbulent stresses  $\overline{u'_i u'_j} \sim \mathcal{O}(\delta^4)$ , hence **not** modeled
- Solutions
  - Clark model / tensor-diffusivity model with eddy viscosity
  - Higher-order gradient model
- Current work
  - Approach #1, as a pilot for #2

## Numerical setup

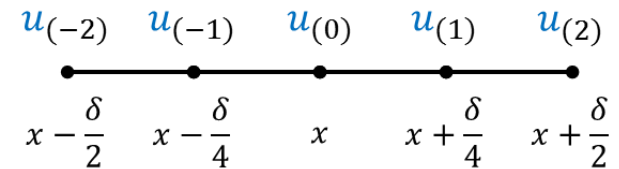
- Discretization of model

- Boole's numerical integration rule (1D)

$$\bar{u} = \frac{1}{\delta} \int_{x' = x - \frac{\delta}{2}}^{x + \frac{\delta}{2}} u(x') dx'$$

$$= \frac{7}{90}u\left(x - \frac{\delta}{2}\right) + \frac{32}{90}u\left(x - \frac{\delta}{4}\right) + \frac{12}{90}u(x) + \frac{32}{90}u\left(x + \frac{\delta}{4}\right) + \frac{7}{90}u\left(x + \frac{\delta}{2}\right) + \mathcal{O}(\delta^6)$$

$$= \sum_{l=-2}^2 \alpha_{(l)} u_{(l)} + \mathcal{O}(\delta^6)$$



- Subfilter-scale model

$$\tau_{11} = \overline{uu} - \bar{u}\bar{u} = \sum_{l=-2}^2 \alpha_{(l)} u_{(l)}^2 - \left[ \sum_{l=-2}^2 \alpha_{(l)} u_{(l)} \right]^2 + \mathcal{O}(\delta^6)$$

- Extension to 3D: sum in each direction, using  $5^3$  points
- Choice of filter length:  $\delta = 4h$

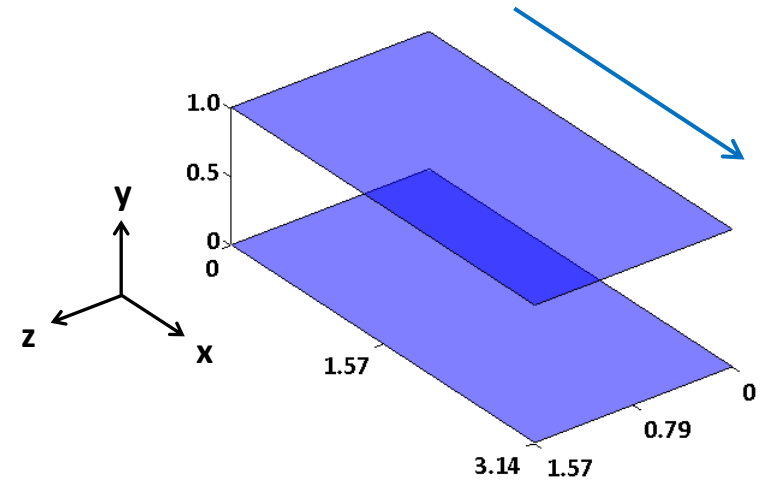
## Numerical setup

- Discretization
  - Finite-volume method on a staggered grid
  - Explicit second-order accurate time-stepping method
  - Fourth-order symmetry-preserving spatial discretization
  - Higher-order gradient model discretization



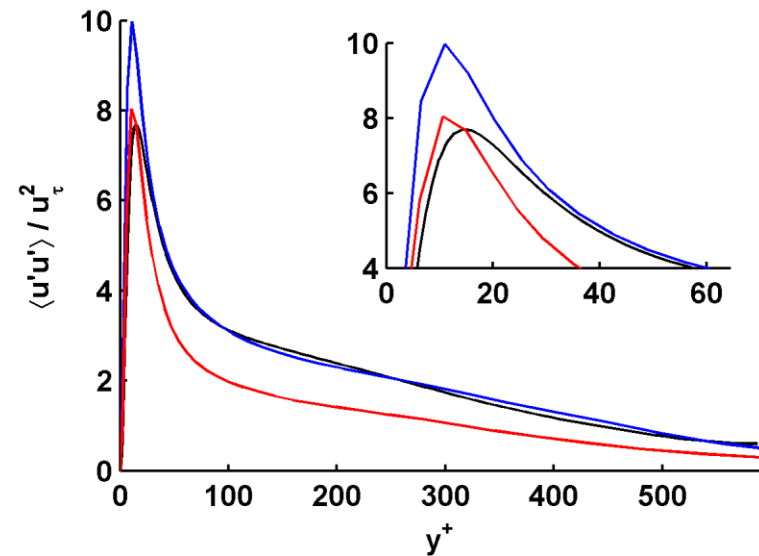
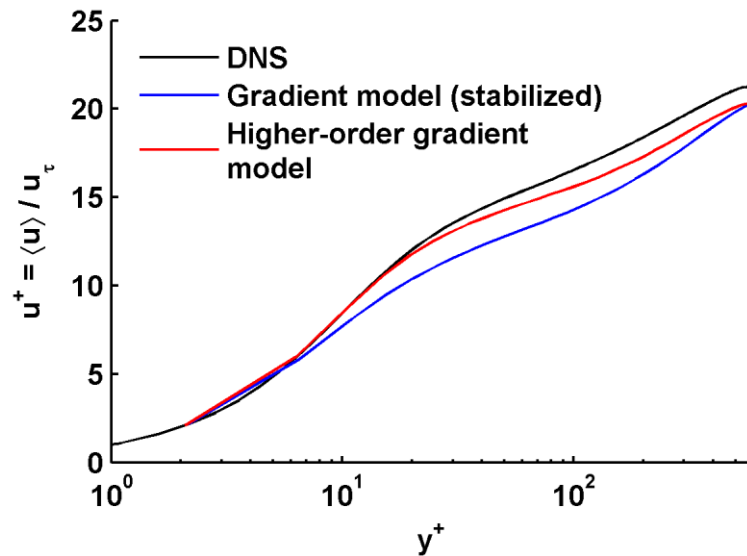
## Numerical test case

- Plane-channel flow
  - Periodic in  $x$  and  $z$ -directions
  - Mass flow prescribed
  - Friction Reynolds number  $Re_\tau = 590$
- Grid
  - LES:  $64^3$  nonuniform grid for a  $\pi * 1 * \pi/2$  channel compared to
  - DNS:  $384 * 257 * 384$  grid



## Numerical results

- Numerical results
  - Velocity profile:  $u^+$
  - Reynolds stress profile:  $\langle u'u' \rangle$



## Conclusions & Future work

- The higher-order gradient model
  - approximate deconvolution method
  - no model constant
  - error smaller than the turbulent stresses
  - tested in a pilot study (approach #1)
  - numerically stable (so far)
- Future work
  - perform stability analysis of model equations
  - reduce the number of points ( $5^3$ ) used in the discretization
  - use the ‘true’ deconvolution model  $\tau_{ij}(\bar{u}_k)$  (approach #2)

Thank you for your attention!



university of  
 groningen

faculty of mathematics  
 and natural sciences

johann bernoulli institute for  
 mathematics and computer science

## Model equations

- Filtered Navier-Stokes equations

$$\frac{\partial \bar{u}_i}{\partial x_i} = 0$$

$$\frac{\partial \bar{u}_i}{\partial t} + \frac{\partial}{\partial x_j} (\bar{u}_i \bar{u}_j) = -\frac{\partial \bar{p}}{\partial x_i} + \frac{1}{Re} \frac{\partial^2 \bar{u}_i}{\partial x_j \partial x_j} - \frac{\partial}{\partial x_j} \underbrace{(\overline{u_i u_j} - \bar{u}_i \bar{u}_j)}_{\tau_{ij}}$$

- Model equations (approach #1)

– Drop bars

$$\frac{\partial v_i}{\partial x_i} = 0$$

$$\frac{\partial v_i}{\partial t} + \frac{\partial}{\partial x_j} (v_i v_j) = -\frac{\partial q}{\partial x_i} + \frac{1}{Re} \frac{\partial^2 v_i}{\partial x_j \partial x_j} - \frac{\partial}{\partial x_j} \underbrace{\tau_{ij}(v_k)}_{\#1}$$

## The higher-order gradient model

- Approach #1 with box filter

$$\begin{aligned}
 \tau_{ij} = & \frac{1}{12} \delta^2 \left[ \frac{\partial u_i}{\partial x_1} \frac{\partial u_j}{\partial x_1} + \dots \right] \\
 & + \frac{1}{1440} \delta^4 \left[ \begin{aligned}
 & 2 \frac{\partial^2 u_i}{\partial x_1^2} \frac{\partial^2 u_j}{\partial x_1^2} + \dots && \text{Pure second derivatives} \\
 & 10 \frac{\partial^2 u_i}{\partial x_1 \partial x_2} \frac{\partial^2 u_j}{\partial x_1 \partial x_2} + \dots && \text{Mixed second derivatives} \\
 & 3 \frac{\partial u_i}{\partial x_1} \frac{\partial^3 u_j}{\partial x_1^3} + \dots && \text{Pure third derivatives} \\
 & 5 \frac{\partial u_i}{\partial x_1} \frac{\partial^3 u_j}{\partial x_1 \partial x_2^2} + \dots && \text{Mixed third derivatives}
 \end{aligned} \right] \\
 & + \mathcal{O}(\delta^6)
 \end{aligned}$$

## The higher-order gradient model

- Approach #2 with box filter

$$\begin{aligned} \tau_{ij} = & \frac{1}{12} \delta^2 \left[ \frac{\partial \bar{u}_i}{\partial x_1} \frac{\partial \bar{u}_j}{\partial x_1} + \dots \right] \\ & + \frac{1}{1440} \delta^4 \left[ \begin{aligned} & 2 \frac{\partial^2 \bar{u}_i}{\partial x_1^2} \frac{\partial^2 \bar{u}_j}{\partial x_1^2} + \dots && \text{Pure second derivatives} \\ & 10 \frac{\partial^2 \bar{u}_i}{\partial x_1 \partial x_2} \frac{\partial^2 \bar{u}_j}{\partial x_1 \partial x_2} + \dots && \text{Mixed second derivatives} \\ & -2 \frac{\partial \bar{u}_i}{\partial x_1} \frac{\partial^3 \bar{u}_j}{\partial x_1^3} + \dots && \text{Pure third derivatives} \end{aligned} \right] \\ & + \mathcal{O}(\delta^6) \end{aligned}$$